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DEVICE FOR DETERMINING THE VALUE OF THE STEADY-STATE ELECTRICITY IN THE PRIMARY CIRCUIT USING A REED SWITCH AND A MICROPROCESSOR

Abstract: This article discusses an innovative device designed to determine the value of the steady-state current in the primary circuit of electrical installations using reed switches and a microprocessor without the use of current transformers. The typical structure of relay protection devices is considered. The main elements are presented.

When choosing a primary converter, a reed switch was taken, because it has certain advantages over current transformers. As part of the research, experimental installations for measurements were assembled. They made it possible to emulate the real conditions in which the relay protection devices have to function, unnecessary and to depict the characteristics of future devices.

The code is presented that allows the microprocessor device to function according to the laid down algorithm. A device on a reed switch and a microprocessor is presented, which allows transmitting a certain amount of current in the primary circuit in digital form (binary code) to the microprocessor protection. The presented measuring device made it possible to implement a method for determining the magnitude of the steady-state short-circuit current.

Keywords: Relay protection, reed switch, microprocessor, identification, current transformer, short circuit.

Introduction

Relay protection devices (RP), designed to detect and disable faults on electrical installations, have a typical structure in accordance with Figure 1, which is divided into measuring (MP), logical (LP) and control (CP) parts. The MP is responsible for the state of the protected electrical installation and issues a signal to the LP when damage occurs. LP receiving a signal from the MP, it executes its logic program and sends a signal to the MP, which is necessary to actuate the switch, etc., amplifying the signal from the LP. Current information is traditionally obtained using current transformers (TC) [1].

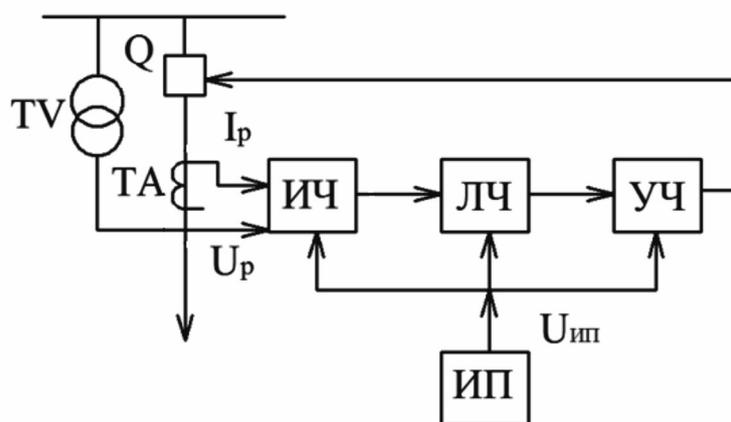


Fig. 1. Typical structure of relay protection devices

At the same time, work is underway [2-5] on the use of magnetosensitive elements for relay protection without TA, which, in turn, are very metal-consuming, distort information when the cores are saturated and create high voltages in secondary circuits when they are broken. As noted at the International Conference on Large Energy Systems (CIGRE) [6], because of these shortcomings, such work is currently relevant. Now it is difficult to give preference to any solution, since most of the work is still far from completion. Relay protection on magnetically sensitive contacts (MK) – reed switches [5-9], which are widely used in technology [10, 11], has development prospects [11, 12]. Some important advantages for RE over other magnetosensitive elements are described in [7-9]. One of the key points is the way to identify the current curve using a reed switch and a microprocessor.

According to the chosen method [13], information about the current in the conductor can be obtained using a reed switch. To determine the magnitude of the steady-state AC short-circuit current, the microprocessor performs the following operations: time measurement t_1 closed state of the reed switch; definition I_m according to the previously entered formula - the approximated dependence $I_m = K_{ИП} \cdot I_{mK}^K = K_{ИП} \cdot f(t_1^K)$, which was taken in the laboratory using CI. The microprocessor allows you to add a software block for comparing a certain current value with the pickup setting. And when the output relay is connected and the setpoint is exceeded, a signal can be sent to it. When measuring the time of the closed state of the reed switch contacts, as is known [13, 14], an accuracy of $1 \mu s$ is required to reduce the errors in determining the magnitude of the current.

For an experimental study of the device on a reed switch and a microprocessor, an installation with a conductor was assembled in accordance with Figure 2.

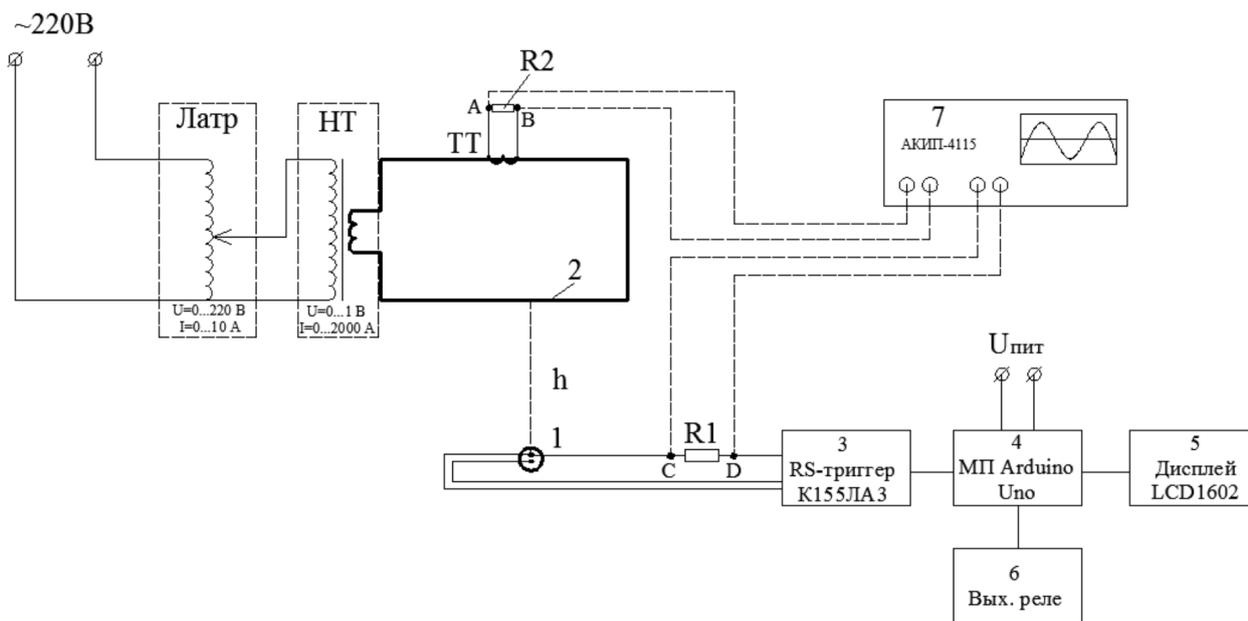


Fig. 2. Installation for creating short-circuit currents

In the installation, an autotransformer (LATR) RNO-250-10 [15] is connected to the 220V supply network, with the help of which the value of the flowing current in the conductor 2 was regulated, which serves as a load transformer. The current lead 2 is connected to the wound winding on a toroidal CT. The winding is made of 8 turns of a cable with a cross section of 95 mm² connected in parallel. In this setup, an alternating current of up to 2000 A was passed through conductor 2. Reed switch 1 was located at a safe distance h from conductor 2. All measurements were monitored using an AKIP-4115 digital oscilloscope. One probe was connected to a low-impedance resistor R1, which was connected in series between the reed switch 1 and the anti-bounce circuit 3, and the second probe was connected to a low-impedance resistor R2 connected to the output of the secondary winding of the measuring current transformer TT (TTE125-4000 / 5A, accuracy class 0.5) through the window of which the conductor 2 passes. The following elements belong to the device. Reed switch 1, the contacts of which are connected to anti-bounce circuit 3, which is made on the RS flip-flop. It is assembled on the basis of the common K155LA3 microcircuit. The signal about actuation and dropout from anti-bounce circuit 3 is fed to the discrete input of the connected microprocessor 4. As microprocessor 4, an Arduino Uno board based on ATmega 328p is taken. When the reed switch contacts bounce, the microprocessor manages to measure the duration of the arising pulses, which leads to false results. To avoid this, circuit 3 is used. The microprocessor is powered from a 5V constant voltage source. By means of a loop, a display 5 LCD1602 is connected to the microprocessor 4 to display information about the determined value of the steady-state current. The block implemented in software additionally compares a certain value with a setpoint. When it is exceeded, a signal is sent to the output relay 6, which is connected to the discrete output of the microprocessor 4. The contacts of the output relay 6 can switch the signal either to the blinker or to the trip coil of the circuit breaker of the protected electrical installation.

On the installation for creating short-circuit currents when the reed switch is located at a safe distance of 100 mm, the multiplicity K (the ratio of the amplitude of the current to the operating current of the reed switch) does not exceed 3. To study the operation of the device at large multiplicity, the installation was assembled in accordance with Figure 3 using the KI. In the installation, an autotransformer (LATR) 2M is connected to the

220V supply network. On the regulated side of the autotransformer, a circuit of two series resistors R2, R3 and an inductor 2 KI (LK >> RK) with a reed switch 1 located inside it is connected. The current in KI 2 and the operation of reed switch contacts 1 is monitored using a digital oscilloscope AKIP-4115 [sixteen]. The first probe is connected to resistor R2, which is located between KI and R3. The second probe to the resistor R1, which is connected in series in the circuit between the reed switch 1 and anti-bounce laughter 3. Further, the elements correspond to Figure 2. In a laboratory installation with a KI, in which a reed switch is located, when a current of 3 A flows in it, the multiplicity K=50 for KEM-3, and for KEM-2 K=80.

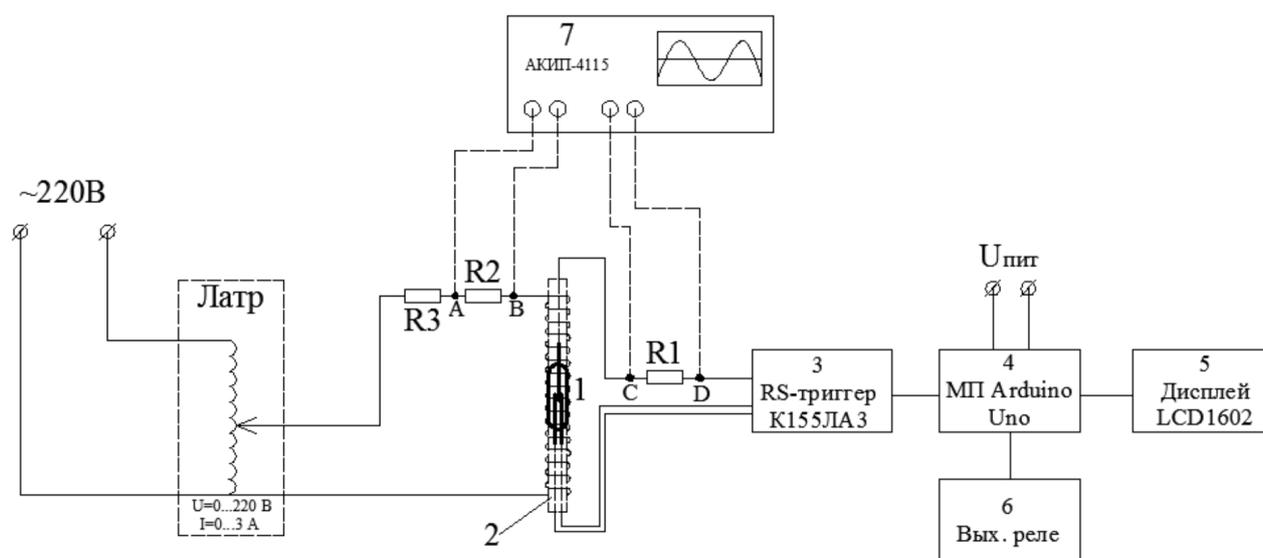


Fig. 3. Installation with KI

The device on a reed switch and a microprocessor, due to the presence of a program unit for comparison with a setting and an output relay, allows to obtain a measuring device for current protection. An experimental model of the measuring device is shown in accordance with Figure 4.

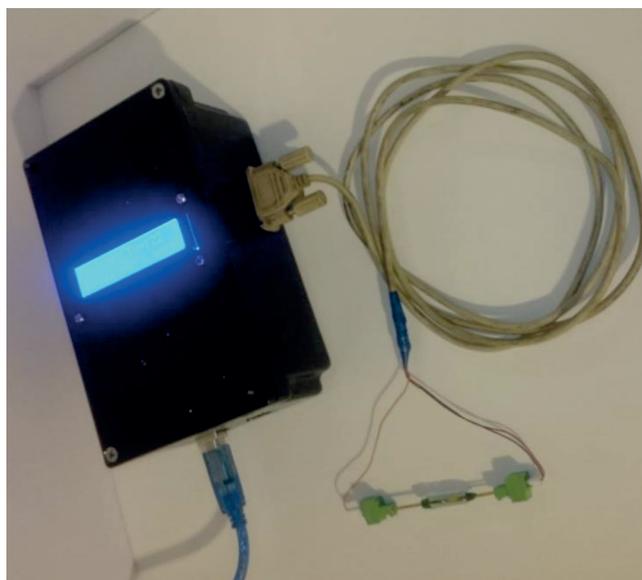


Fig. 4. Photo of the measuring body

The program that operates in the measuring body is as follows:

```

unsigned long t1; // introduce variables
float Im;
float a0=-2,318;
float a1=3,493;
float a2=-2,309;
float a3=0,879;
float a4=-2,128;
float a5=3,39;
float a6=-3,56;
float a7=2,376;
float a8=-9,147;
float a9=1,549;
#include<LiquidCrystal.h>// connect the library to work with the display
LiquidCrystal lcd(7, 8, 9, 10, 11, 12);
void setup() {
  pinMode(2, INPUT); // configure ports for reading
  pinMode(13, OUTPUT); // configure ports for recording
  Serial.begin(9600);
  lcd.begin(16, 2);// loading screen
  lcd.print("Loading");
  delay(500);      // wait 0.5 seconds
  lcd.print("");
  delay(500);      // wait 0.5 seconds
  lcd.print(".");
  delay(500);      // wait 0.5 seconds
  lcd.print("");
  delay(1000);     // wait 1 seconds
  lcd.clear();     // clearing the screen}
void loop() {
  t1 = pulseIn(2,HIGH);// closed time measurement
  // determine the current value by measuring time
  Im = a0·(pow(10,6))+a1·(pow(10,3))·t1+a2·(pow(t1,2))+a3·(pow(10,-3))·(pow(t1,3)) +a4·(pow
(10,-7))·(pow(t1,4))+a5·(pow(10,-11))·(pow(t1,5))+a6·(pow(10,-15))·(pow(t1,6))+a7·(pow(10,
-19))·(pow(t1,7))+a8·(pow(10,-24))·(pow(t1,8))+ a9·(pow(10,-28))·(pow(t1,9));
  If (Im > 500)// output trigger condition
  {
  digitalWrite(13, HIGH);// output trigger
  }
  else
  {
  digitalWrite(13, LOW);// output failure
  Serial.println(t1);// we display the value of the closed time. comp. on PC
  Serial.println(Im);// display the current value on the PC
  // display information on the display
  lcd.setCursor(0, 0);// set the cursor to the 0th column, 0th row
  lcd.print("t1=");
  lcd.print(t1);// display the measured time
  lcd.setCursor(0, 1);// set the cursor in the 0th column, 1st row

```

```
lcd.print("Im=");  
lcd.print(Im);// display the current value  
} End of the program.
```

Characteristics of the current protection measuring device.

The performance is estimated from the following considerations. To determine the value of the steady-state short-circuit current in the conductor, it is necessary to measure the time of the closed state of the reed switch, therefore, when a short-circuit occurs, the reed switch must close and open. The time t_1 of the closed state of the reed switch cannot exceed 0.01 s, we will designate it as the time t_H of the measurement. After measuring t_1 , the microprocessor performs mathematical operations, assignment and comparison operations. The number of operations in the algorithm does not exceed 50, the microprocessor performs them in one cycle, which lasts no more than 0.001 s, let us designate its time t_U of the cycle execution. And the operation of the output relay remains, which for high-speed relays does not exceed 0.01 s, we will designate as t_P . Thus, the performance is estimated by the formula

$$t_{OTKI} = t_H + t_U + t_P = 0,021 \text{ s.}$$

The device on the reed switch and the MP allows transmitting in digital form (binary code) to the microprocessor protection a certain amount of current in the primary circuit. The presented measuring device in accordance with Figure 4 made it possible to implement a method for determining the value of the steady-state short-circuit current.

Conclusion

A reed switch located near the current conductor of an electrical installation and a microprocessor make it possible to determine the value of the steady-state short-circuit current in the primary circuit with an error $\leq 10\%$ with its multiplicity $K \leq 80$. To do this, you need to measure time t_1 the closed state of the reed switch contacts and in the microprocessor determine the value I_m current in the conductor from the formula $I_m = K_{ПП} \cdot I_{mK} = K_{ПП} \cdot \sum_{n=0}^n an \cdot (t_1^K)^n$, obtained after approximation of the dependence $I_{mK} = f(t_1^K)$ taken in laboratory conditions using IC ($L_K \gg R$, L_K – winding length, R – loop radius). In the formula I_{mK} – current in the inductor coil (IC); t_1^K – the same time as t_1 (only when the reed switch is located in the IC); $K_{ПП}$ – conversion factor I_m from the magnitude I_{mK} ; n – degree of approximating polynomial.

The developed device on a reed switch and a microprocessor implements a method for determining the value of the steady-state short-circuit current. When adding a program block for comparing a certain current value with a setting and an output relay, the device performs the functions of a current protection measuring device, which does not need information from a current transformer. The code of his program is presented. The performance is estimated at 21 ms.

Gratitude

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